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Nutrient recovery from piggery effluents

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SUMMARY

The present study aims to evaluate struvite precipitation potential, using the Visual MINTEQ modelling package. A solution speciation model of struvite precipitation in different phases has been developed. This model indicates that across a wide range of pH (6-14) various other crystals are formed along with struvite, whereas struvite formation is dominant in the pH range of 7.75-9.27. Solution speciation modelling indicates that a Magnesium Ion Selective Electrode can be used to infer struvite supersaturation, enabling better modelling and control of crystal growth kinetics. A brief thermodynamic investigation on piggery wastewater collection pond will be performed using this model.

Key words: struvite, Visual MINTEQ, ion selective electrode, supersaturation, solid phases.

1. INTRODUCTION

High nutrient loads from piggery effluents have implications for several environmental concerns, including soil acidification, eutrophication in water bodies, and burning of tree roots due to the over application of nitrogen. It is well known that struvite is formed in wastewater streams that are supersaturated, leading to significant maintenance costs. The main forms of nutrients are magnesium, ammonium and phosphate. Von Munch and Barr [1] report that it is possible to recover nutrients from nutrient-rich wastewater streams. The key feature of this technique is the combined removal of ammonium and phosphate instigated by the addition of magnesium ions. The synthetic formation of struvite is expressed by below [2]:

$$Mg^{2+} + NH_2H_2PO_4 + 6H_2O \rightarrow MgNH_4PO_4 \cdot 6H_2O + H^+ (1)$$

Performing batch kinetics experiments requires maintenance of constant supersaturation, in order to determine its effect on crystal growth rates. A solution speciation model, using Visual MINTEQ (version 2.11) for example, enables detailed assessment of struvite crystallization potential. This program is based on the MINTEQA2 version 4.0. The original version of MINTEQ was developed at Battelle Pacific North Western Laboratory (PNL) by combining the fundamental mathematical configuration of MINTEL with WATEQ3 [3].

This paper reports on the use of solution speciation modelling, using Visual MINTEQ in order to further improve our understanding of struvite solution thermodynamics. This is an important first step in developing process models for nutrient recovery systems design and control.

2. DATABASE MANAGEMENT IN VISUAL MINTEQ

The default database of Visual MINTEQ does not contain struvite as a supersaturated solid phase. The initial task therefore is to add struvite into the Visual

MINTEQ database. The basic assumption of this model is the insignificant effect of infinite solid phases, finite solid phases and possible solid phases. To include the struvite in the database, Mg^{2+} , NH_4^+ and PO_4^{3-} ions were added to the input data file at constant pH (8.5), along with ionic strength, which is calculated via mass balance. The concentration of the incorporated solution composition was recorded in mg/L. The required values for augmenting the default solid phase list in Visual MINTEQ, are Log K, preferred species name, rate of change of enthalpy, charge of species, number of components and their name, along with stoichiometric composition ratios. The suggested ID and gram molecular weight of anhydrous struvite are 2000021 and 137, respectively. This database modification was compiled using the change of enthalpy, dH_r , at zero. The value of a change in enthalpy is used to adjust the equilibrium constant for temperatures other than $25^{\circ}C$. The values supplied in Visual MINTEQ's thermodynamic database are referenced to a temperature of 25°C. A new set of equilibrium constants is calculated before solving the equations. If the standard enthalpy change is not available in the database, MINTEQ uses the uncorrected $Log\ K\ (25^{\circ}C)$. However, no change of enthalpy was put into practice since the temperature of the effluent collection pond in an open environment would be close to this point. The value of Log K, used in Visual MINTEQ, refers to the logarithmic value of the equilibrium constant of reaction. For solids, the equilibrium constant of reaction, K, is reciprocal to the solubility product value (K_{sp}) , sand hence the value recommended in the Visual MINTEQ database management is the negative logarithmic value of the solubility product i.e., $-Log K_{sp}$ [3]. Proposed values of $-Log K_{sp}$ from previous researchers are found in Table 1.

Table 1 Suggested value of -Log K_{SD} by previous researchers

Recommended by	-Log K _{sp}
Bube [4]; Snoeyink and Jerkins [5]	12.6
Taylor et al. [6]; Nelson [7]; Abbona [8]	13.15
Burns and Finlayson [9]	13.12
Ohlinger [10]	13.27

It is felt that Ohlinger's work [10] represents the most comprehensive treatment of this system. For this reason we employed a value of 13.27 for - $Log K_{sp}$ in our Visual MINTEQ input file. A priority order for thermodynamic stabilities of each solid is established by comparing the appropriate ion activity products (IAP) with the corresponding formation constant, after the aqueous phase has been equilibrated [3]. The saturation index (SI) for each solid is defined as:

$$SI = Log(IAP) - LogK_s$$
 (2)

where Ks is temperature corrected solubility constant.

The database system allows the solid phase to be formed when the solution is supersaturated indicating that the value of Saturation Index (SI) is greater than zero. For the equilibrium phase and undersaturated solution, the value of SI remains zero or less than zero.

3. FORMATION OF OTHER CRYSTALS

To investigate the influence of pH on struvite precipitation, the constituents of struvite, (i.e., Mg^{2+} , NH_4^+ , PO_4^{3-}) were introduced into a Visual MINTEQ input file at pH values ranging from 6 to 14. The input concentrations of Mg^{2+} , NH_4^+ , and PO_4^{3-} were 348, 261 and 1790.75 mg/L, respectively. This approach allows struvite or other crystals to form, either in undersaturated or supersaturated form. When the model is allowed to precipitate the supersaturated solids are formed in the solution. Table 2 highlights the potential solid phases that can result. It should be noted that struvite had to be added to the database as a solid, since it was not in the default database. Along these lines, it is possible that other solid phases might appear, but will not, since they are not defined in the database.

Figure 1 shows different types of solids formed in the solution, predicted by Visual MINTEQ. Struvite formation dominates through the range of pH 7 to 10.5, and in the pH range of 7.75 to 9.27 struvite should be the only crystal that is formed, based on the chemical species assumed to be present. Below pH 6.75 or above 9.27 other crystals such as Newberyite, Brucite, and Farringtonite are formed, which reduces the amount of struvite formed. Therefore, the possible solids formed depend on the pH of the solution, which in turn alters the supersaturation of the solution. Based on ionic activity product, generated by the degree of supersaturation, different types of crystals will form. The formations of different types of crystal depend solely on the equilibrium constants, which are described in Table 1. As soon as the ion activity product (IAP) exceeds the minimum equilibrium constant of solubility, crystals appear in the solution. When the solution's Log (IAP) exceeds 13.27, struvite formation is precipitated, which is signified in the pH range 7-11 (Figure 1).

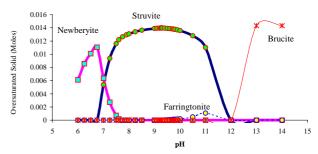


Fig. 1 Solids in a supersaturated solution

In the literature, the apparent pH for the minimum solubility has been documented as between 9.0 to 11.0 [5, 10-13]. Ohlinger [10] acknowledge that the pH for the minimum solubility of struvite is 10.3, whereas it has previously been suggested as 10.7 [5, 12]. Buchanan et al. [11] reported the minimum value of pH for struvite solubility was 9.0. Doyle et al. [13] demonstrated that the minimum solubility of struvite occurred at pH 9.0 to 10.0, with the struvite precipitation commencing at 7.5. Buchanan et al. [11] observed the range of pH at which struvite forms was 7.0 to 11.0. Doyle et al. [13] documented that struvite precipitation was highly unlikely below pH 7.88 although pH 7.5 resulted in the definite reduction of nutrient composition. It is therefore recommended by Doyle et al. [13] to use pH 8.0 for favourable precipitation and 8.83 for rapid struvite precipitation.

Table 2 Logarithmic activity product of different solid phases

Product name	Chemical Composition	Log (IAP) = Log (Mg2+.PO43NH4+)		
Brucite	$Mg(OH)_2$	-16.84399		
Active Mg (OH) ₂	$Mg(OH)_2$	-21.58409		
Periclase	MgO	-18.794		
Farringtonite	$Mg_3(PO4)_2$	23.28		
Newberyite	$MgHPO_4.3H_2O$	18.175		
Struvite	$MgNH_4PO_4$	13.27		

4. INFLUENCE OF COMPOSITION ON STRUVITE FORMATION

The main purpose of this modelling is to determine the optimum conditions for struvite formation. The presumed optimum pH is deemed to be 8.5 from the previous section in this paper. The input data in the Visual MINTEQ input file is 1:x:y, which expresses the ratio of NH_4^+ , Mg^{2+} , PO_4^{3-} by means of a fixed NH_4^+ concentration of $261 \ mg/L$ and variable amounts of Mg^{2+} and PO_4^{3-} . A constant level of NH_4^+ ion is used, due to its disinclination to form complexes [10], which in turn maintains the fairly stable ionic activity. The precise forms of complexes of different components are presented in Table 3.

Table 3 Dissolved and adsorbed species presence in struvite system

Components	Complexes
$PO_4^{\ 3}$	PO_4^{3-} , $MgHPO_4$ (aq), $MgH_2PO_4^{+}$,
	HPO_4^{2-} , $H_2PO_4^{-}$, $MgPO_4^{-}$
$NH_4^{I^+}$	NH_4^+ , NH_3 (aq)
Mg^{2+}	Mg^{2+} , $MgH_2PO_4^+$, $MgHPO_4$ (aq),
	$MgOH^{+}, MgPO_{4}^{-}$

Due to the presence of different complexes of Mg^{2+} and PO_4^{3-} , the solution ionic activity depends solely on their composition at constant pH. Figure 2 represents the trend of struvite formation at variable Mg^{2+} and PO_4^{3-} compositions, at pH of 8.5.

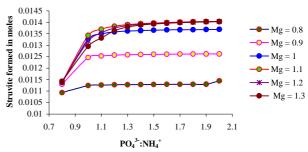


Fig. 2 Influence of composition on the struvite formation

Figure 2 shows that a suitable composition ratio of ammonium, magnesium and phosphate ion is:

$$NH_4^+: PO_4^{3-}: Mg^{2+} = 1:1.1:1.3$$

5. ION SELECTIVE ELECTRODE

Two types of experimental configurations, either constant pH or constant supersaturation, would usually be implemented for struvite reactor design purposes [14]. It has been proposed that semi-batch precipitation with constant supersaturation is more efficient than the constant pH case [14].

Bouropoulos and Koutsoukos [15] dealt with this scheme using mechanically coupled burettes from an automatic titrator to maintain constant pH, as well as constant composition, which in turn maintained a constant supersaturation conditions. The approach of the present investigation will use magnesium Ion Selective Elective (ISE) along with a pH controller to maintain a constant level of supersaturation. Two types of ion selective electrodes, a magnesium ion selective electrode and an ammonium ion selective electrode, are considered in this investigation. Based on the Visual MINTEQ modeling, the following two difficulties have been identified in selecting a more suitable ISE:

- 1. Percentage of available free ions, and
- 2. Interference from other ions.

5.1 Percentage of available free ions

The sensitivity of a particular ISE depends on the level of free ions present in the solution. Ionic concentrations of Mg^{2+} , NH_4^+ and PO_4^{3-} at 348, 257 and $304 \, mg/L$ were introduced in the Visual MINTEQ input file at different pH and temperature levels. It is worth pointing out that $MgCl_2$ and $NH_4H_2PO_4$ were used in batch experiments as the source of Mg^{2+} and NH_4^+ , respectively. Figures 3 and 4 are developed from Visual MINTEQ output data, showing the levels of free ionic concentrations for ammonium and magnesium. Clearly the percentage of free Mg^{2+} is much greater than that of NH_4^+ , which varies strongly with varying pH and temperature levels.

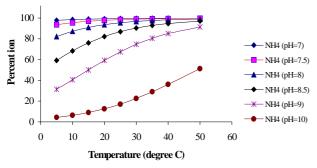


Fig. 3 Free NH_4^+ in various conditions

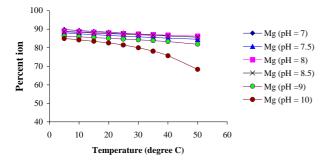


Fig. 4 Free Mg²⁺ in various conditions

5.2.1 Interference from other ions

Another problem of the ISE measurement is the effect of interference from other ions, since many ISEs are non-specific and sensitive to other ions to some extent. This effect could be adverse for a real effluent where various types of chemicals exist in the mother liquor. The interference of wide varieties of ions with the mother constituents of struvite could reduce ionic strength and activity of the solution relative to its true values, particularly at high concentrations. In very dilute solutions these interferences are ineffective in influencing the efficiency of the Magnesium ISE. The key interferences on Magnesium ISEs are considered in this modelling include Cu^{2+} , Zn^{2+} , Ni^{2+} , Fe^{2+} , Na^+ , K^+ and Ca^{2+} . The consequence of interference is defined by:

$$IA = C/C' \tag{4}$$

where:

IA - Interference ratio,

C - Concentration of interfering ion in molarity,

C' - Concentration of measured ion in molarity.

To identify the interference of Mg^{2+} with other ions, such as Cu^{2+} , Zn^{2+} , Ni^{2+} , Fe^{2+} , Na^+ , K^+ , Ca^{2+} , the main component of struvite was inserted in Visual MINTEQ input file along with the interference ion with variable concentrations. The concentration of Mg^{2+} , NH_4^+ and PO_4^{3-} are 348, 257 and 304 mg/L, respectively at a temperature of 25° C. The model was simulated at pH 8.5. The selected output of the model, describing the effect of various ions on Mg^{2+} more precisely, is represented in Table 4. Significant interference between Mg^{2+} and other ions is observed

when the interference ratio is 1.437 or greater, i.e. at strong concentration of interferring ions, particularly for Ca^{2+} and Fe^{2+} . The interference of other ions, remaining in wastewater, are less significant. However, the concentration of Ca^{2+} and Fe^{2+} is unlikely to exceed the concentration of Mg^{2+} . The complexes of PO_4^{3-} , NH_4^+ and Ca^{2+} are $CaPO_4^-$, $CaNH_3^{2+}$, CaHPO₄ (aq), CaNH₃²⁺, CaPO₄, CaH₂PO₄⁺, which increase the free ion concentration of magnesium. This setback affects the ionic strength of the solution, reducing the measured activity relative to the true concentration of magnesium, and corrupts measurements of true readings. However, for the solution of diluted interfering ions, this complexity is rather insignificant and can be ignored due to a constant level of percentage free Mg^{2+} ion (Table 4).

Table 4 Influence of interferent on magnesium ion

Interferent (mg/L)	Molar ratio of interfer. ions and Mg ²⁺ ion	$% Mg^{2+}$ (Interferent = Ca^{2+})	$% Mg^{2+}$ (Interferent = Na^+)	$% Mg^{2+}$ (Interferent = Fe^{2+})
0	0	85.145	85.145	85.145
30	0.0862	85.893	85.232	86.319
100	0.287	87.319	85.431	88.653
500	1.437	92.137	86.471	94.971

6. POND INVESTIGATIONS

Piggery wastewater contains diverse types of nutrients. The investigation of piggery wastewater was carried out in different types of pond in one of the Queensland's pig farms. The summary of a survey is represented in Table 5.

The possibility of different solids formation in wastewater is performed in the abovementioned piggery wastewater pond. The sample was collected from the primary pond (P), the secondary pond (S) and the final irrigation pond (F) at a pH 7.9, 8.0 and 7.8, respectively. The solutions were collected from the pond surface and were filtered to remove suspended matters. The solutions were chemically analysed using standard methods of chemical analysis for the cited ions. The investigation was performed for major and minor nutrients. A solution speciation model using Visual MINTEQ was employed across a wide range of pH. The existing database in Visual MINTEQ modelling was modified for struvite and Magnesium Potassium Phosphate using the thermodynamic data presented in Table 6.

The value of the saturation index (SI) in Table 7 represents the solution characteristics based on their solubility. It is worth pointing out that SI>0 and SI<0 express supersaturated solid and undersaturated solid situations, respectively, while a value of SI=0 represents the chemical equilibrium. The wastewater of the primary, secondary and final irrigation ponds

Table 5 Characteristics of piggery wastewater, surveyed in Queensland (Concentration in mg/l)

Ponds	pН	Ca^{2+}	Cu^{2+}	Fe^{3+}	$K^{^{+}}$	Mg^{2+}	Mn^{3+}	$NH_4^+ N$	$PO_4^{3-}P$	SO_4^{2-}	Na^+
P	7.9	11.2	0.20	0.59	823.2	22.3	0.01	244.5	7.80	46.3	696.0
S	8.0	7.70	0.17	0.76	982.0	19.5	0.01	223.1	5.0	56.7	790.4
FI	7.8	12.7	0.22	0.98	718.6	20.6	0.01	162	8.90	48.8	676.2

Footnote: P = Primary Pond, S = Secondary Pond, FI = Final Irrigation Pond

Table 6 Thermodynamic data for database management

Name of Crystal	Delta_h	Log_K
Struvite	0	-13.27
$(Mg: NH_4: PO_4: H_2O = 1:1:1:6)$	U	[10]
MKP	0	-10.6197
$(Mg: K: PO_4: H_2O = 1:1:1:6)$	U	[6]

Table 7 Saturation index (SI) of different solids for the piggery pond under evaluation

1 0.	5 · · / F					
Types of	pН	Brucite	HAP	MKP	MnHPO4	MAP
Pond						
Primary	7.9	-4.4	0	-24.26	0	-27.11
Primary	8.5	-3.2	0	-23.63	0	-26.54
Primary	10.7	0	0	-22.58	0	-26.82
Secondary	8.0	-4.3	0	-24.36	0	-26.93
Secondary	8.5	-3.3	0	-23.85	0	-27.34
Secondary	10.7	0	0	-22.57	0	-26.87
Final	7.8	-4.6	0	-24.37	0	-27.35
Irrigation	7.0	-4.0	U	-24.37	U	-27.33
Final	8.5	-3.2	0	-23.64	0	-26.66
Irrigation	0.5	-3.2	U	-23.04	U	-20.00
Final	10.7	0	0	-22.57	0	-26.93
Irrigation	10.7	U	U	-22.37		-20.93

in a pig farm remains in a saturated state for HAP (Hydroxyapatite: $Ca_5(PO_4) \cdot 2H_2O$) and $MnHPO_4$ in the wide range of pH, whereas Brucite $(Mg(OH)_2)$ remains in a saturated stage at higher pH. MKP (Magnesium Potassium Phosphate: $MgKPO_4 \cdot 6H_2O$) and struvite (Magnesium Ammonium Phosphate: $MgNH_4PO_4\cdot 6H_2O$) remains undersaturated, owing to low concentrations of magnesium and phosphorus. It is therefore necessary to maintain a higher optimum level of magnesium and phosphorus in order to supersaturate the system to yield struvite crystals. An increase of pH value of the working solution can also trigger struvite crystallization by making it supersaturated. The minimum level of supersaturation of the working solution can be worked out by trial and error method of increasing pH and components concentration (Mg²⁺ and PO₄³⁻) using MINTEQ. It is worthwhile pointing out that the minimum supersaturation at which struvite precipitation takes place varies widely with solution concentrations, i.e. Mg²⁺, NH₄⁺, PO₄³⁻ and other ions. The recovery of phosphorus using struvite crystallization has significance as it removes ammonium and phosphorus simultaneously.

7. CONCLUSION

- 1. The range of *pH* for experiments is proposed to be 7.75 to 9.27, although the suggested optimum *pH* is 8.5. Further experimental investigation is necessary.
- A magnesium Ion Selective Electrode has been identified to be more effective than an ammonium Ion Selective Electrode to infer and control the composition, and therefore supersaturation, of the solution
- 3. The effect of interfering ions is essentially insignificant, since the interfering ions remain in a diluted form both in the synthetic solution as well as in real piggery effluents.
- 4. The solid phases found in this struvite model are Struvite, Brucite, Periclase, Newberyite and Farringtonite. However in the proposed operating range struvite is the dominant solid phase. When struvite is the dominant solid phase in its characterized supersaturated solution, most of the excluded solid phases remain in undersaturated form unless their IAP exceeds the solubility product values, existing in Visual MINTEQ default databases.
- 5. Overall, the use of the solution thermodynamics package, Visual MINTEQ, has assisted greatly in the preliminary design and development of nutrient recovery systems for piggery effluent streams.

8. REFERENCES

- [1] V. Munch, E. and K. Barr, Controlled struvite crystallization for removing phosphorus from anaerobic digester side streams, *Water Resources*, Vol. 35, pp. 151-159, 2001.
- [2] A.E. Durrant, et al., Review of the feasibility of recovering phosphate from wastewater for use as a raw material by the phosphate industry, *Environmental Technology*, Vol. 20, pp. 749-758, 1999.
- [3] J.D. Allison, E.S. Brown and K.J. Novo-Gradac, MINTEQA2/PRODEFA2, A geochemical assessment model for environmental systems: Version 3.0 User Guide, US EPA, Athens, Georgia, 1991.
- [4] K. Bube, Uber Magnesium ammonium phosphate, *Z. Anal. Chem.*, Vol. 49, pp. 525-596, 1910.
- [5] V.L. Snoeyink and D. Jenkins, *Water Chemistry*, John Wiley and Sons, USA, 1980.

- [6] A.W. Taylor, A.W. Frazier and E.L. Gurney, Solubility product of magnesium ammonium phosphate, *Trans. Faraday Soc.*, Vol. 59, pp. 1580-1589, 1963.
- [7] N.R. Nelson, R.L. Mikkelson and D.L. Hesterberg, Struvite formation to remove phosphorus from anaerobic swine lagoon, Proc. of the 8th Int. Symposium on Animal, Agricultural and Food Processing Wastes, Des Mines, 2000.
- [8] F. Abbona and R. Boistelle, Growth morphology and crystal habit of struvite crystal (*MgNH*₄*PO*₄·6*H*₂0), *Journal of Crystal Growth*, Vol. 46, pp. 339-354, 1979.
- [9] J.R. Burns and B. Finlayson, Solubility product of magnesium ammonium phosphate hexahydrate at various temperature, *J. Urol.*, Vol. 128, pp. 426-428, 1982.
- [10] K.N. Ohlinger, Kinetics effects on preferential struvite accumulation in wastewater, PhD thesis, School of Engineering, California State University, California Davis, 1999.

- [11] J.R. Buchanan, C.R. Mote and R.B. Robinson, Thermodynamics of struvite formation, *Trans. Am. Soc. Agri. Eng.*, Vol. 327, No. 2, pp. 617-621, 1994.
- [12] W. Stumm and J.J. Morgan, *Aquatic Chemistry*, John Wiley and Sons, New York, 1996.
- [13] J. Doyle, Fundamental chemistry and control of struvite precipitation, Proc. of the 2nd International Conference on the Recovery of Phosphorus from Sewage and Animal Wastes, Noordwijkerhout, 2001.
- [14] O. Söhnel and J. Garside, *Precipitation: Basic Principles and Industrial Applications*, Butterworth-Heinemann, 1992.
- [15] C.C. Bouropoulos and P.G. Koutsoukos, Spontaneous precipitation of struvite from aqueous solutions, *Journal of Crystal Growth*, Vol. 38, pp. 213, 2000.

POVRAT HRANJIVIH TVARI IZ ISPUSTA OTPADNE VODE S FARME SVINJA

SAŽETAK

Cilj ovog ispitivanja je procijeniti potencijal taloženja struvita koristeći paket za modeliranje Visual MINTEQ. Razvijen je model rješavanja za taloženje struvita u različitim fazama. Ovaj model pokazuje da se za široki raspon pH (6-14) formiraju i različiti drugi kristali zajedno sa struvitom, dok je formiranje struvita dominantno u rasponu pH od 7.75-9.27. Model rješavanja pokazuje da se selektivna elektroda jona magnezija može koristiti za procjenu velikog zasićenja struvitom što omogućava bolje modeliranje i kontrolu kinetike razvoja kristala. Ovaj model će se koristiti za kratko termodinamičko istraživanje bazena za sakupljanje otpadne vode iz farme svinja.

Ključne riječi: struvit, Visual MINTEQ, selektivna elektroda iona, veliko zasićenje, kruta faza.